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Thermodynamic stabilities of strontium and barium cerates using Knudsen effusion quadrupole mass spectrometry

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article info

ABSTRACT

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A Knudsen effusion cell coupled to a quadrupole mass spectrometer was calibrated by measuring the ion intensities of CO_2 ⁺ peak over the phase mixture {BaCO₃(s)+BaO(s)} at different temperatures. The instrument constant (K_{inst}) was calculated by comparing the ion intensities with the partial pressure data for this phase mixture taken from the literature. Subsequently, the ion intensities of CO_2^+ peak over the phase mixture ${SrCO_3(s) + SrO(s)}$ was measured and the partial pressure of $CO_2(g)$ over this phase mixture was calculated using this instrument constant. The enthalpy of reaction ($\Delta_{\rm r}H_{\rm m}{}^{\circ}$) was calculated and compared with the literature data which was found to be in excellent agreement. After validating this method by the above measurements, the partial pressure of $CO₂(g)$ over the equilibrium phase mixtures of ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}$, ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$, ${Sr₂CeO₄(s) + 2SrCO₃(s) + CeO₂(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)}$ were determined as a function of temperature. These partial pressure data were used in conjunction with auxiliary thermodynamic data from the literature to determine the standard molar Gibbs energies of formations of three ternary oxides BaCeO₃(s), SrCeO₃(s) and $Sr₂CeO₄(s)$. The thermodynamic data shows that at a particular pressure of $CO₂(g)$, BaCeO₃(s) is more prone to form BaCO₃(s) as compared to SrCeO₃(s) to form SrCO₃(s). This is an importnat asseseement since these cerates doped with rare-earths are potential proton conducting ceramic oxides used as electrolytes in solid oxide fuel cells.

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1. Introduction

Ceria based ternary oxides of barium and strontium such as $BaCeO₃(s)$ and $SrCeO₃(s)$ have gained much importance due to their wide applications in solid oxide fuel cell (SOFC), hydrogen sensors, hydrogen extractors from gas mixtures, oxygen sensors and inorganic pigments [\[1–5\].](#page-6-0) A SOFC system usually utilizes a solid ceramic as the electrolyte and operates at higher temperature around 800 ◦C. SOFCs consist of two electrodes sandwiched around a hard ceramic electrolyte such as yttria stabilized zirconia [\[6–9\].](#page-6-0) In SOFC, hydrogen is fed into the anode of fuel cell and oxygen from the air enters into the cell through the cathode and the overall cell reaction leads to the formation of $H₂O$. Depending on the type of electrolyte, SOFC can be classified into two types: (1) oxide ion conducting SOFC; (2) proton conducting SOFC. The generation of water on fuel side dilutes the fuel in oxide ion conducting electrolyte and thus decreases the efficiency of the cell. These also require very high operating temperatures (>800 ◦C), consume large energy which is undesirable. To overcome these problems, the concept of proton conducting ceramic oxides has gained much importance as an electrolytic medium. Out of various options, rare-earth doped $SrCeO₃(s)$ and BaCeO₃(s) are found to have high proton conductivities in moist environment. The proton conduction in these ceramic oxides arises due to defect reactions. Proton defects in the oxide are created when the oxide containing oxygen ion vacancies dissociate and absorb water from a surrounding wet atmosphere. In proton conducting SOFCs, water is formed on cathode, i.e. on air side, therefore, dilution of fuel does not occur and operating temperature of these cell is also low compared to oxide ion conducting SOFCs. These proton conducting ceramics such as $BaCeO₃(s)$ and $SrCeO₃(s)$ are very prone to form carbonates even with low concentration of $CO₂(g)$ which in turn decreases their stability. $Sr₂CeO₄$ has luminescence properties when excited with UV light, cathode rays and X-rays [\[10\].](#page-6-0) It has also been established that un-doped and doped $Sr_2CeO_4(s)$ act as efficient blue-white and red phosphor materials [\[11\].](#page-6-0)

A large number of literature reports are available related to the synthesis and thermodynamic stability of these cerates with respect to their constituent binary oxides [\[12–15\]. B](#page-6-0)ut, the stability of these cerates has not been determined with respect to their carbonate formation. In this study, an attempt has been made to study the stability of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) with respect

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to their carbonate formation using Knudsen Effusion Quadrupole Mass Spectrometry (KEQMS).

2. Experimental

2.1. Materials preparation

BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) were prepared using conventional solid state reaction method. Stoichiometric proportions of BaCO₃(s), SrCO₃(s) (LEICO Industries Inc., USA, mass fraction 0.9999) and $CeO₂(s)$ (Indian Rare Earths Ltd., India, mass fraction 0.999) were homogenously mixed using an agate mortar and pestle. The mixtures were pelletized using a tungsten carbide lined steel die at a pressure of 20 MPa. The pellets were first heated at 1100 K for 24 h. Then, the resultant products were ground, again pelletized and further heated at 1200 K for 48 h. The individual compounds were characterized by X-ray powder diffraction technique using STOE powder diffractometer with Cu $K\alpha$ radiation and graphite monochromator and found to be pure crystalline phases of BaCeO₃(s), SrCeO₃(s) and $Sr₂CeO₄(s)$

Chemical analysis of all the synthesized samples was carried out using EDXRF method. The alkaline earth to cerium metal ratio obtained from EDXRF analysis was found to be the same as the formula ratio indicating that the compounds are stoichiometric with respect to metals.

Phase mixtures of ${BaCeO_3(s) + BaCO_3(s) + CeO_2(s)}$, ${SrCeO_3(s) + SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) + CeO_2(s)}$ ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) +}$ $SrCeO₃(s)$ } were prepared by homogenously mixing the individual oxides for KEQMS experiment. The pellets of different phase mixtures were then broken into small pieces and kept in a desiccator for measurement of partial pressures of $CO₂(g)$.

2.2. Knudsen effusion quadrupole mass spectrometry (KEQMS)

In this study, a Residual Gas Analyzer (RGA) based on quadrupole mass spectrometer coupled to a Knudsen effusion system was used for equilibrium partial pressure measurements. The details of the experimental setup and the calibration procedure of the experimental setup have been described by Rakshit et al. [\[16\]. T](#page-6-0)he temperature near the Knudsen cell was measured using a pre-calibrated (ITS-90) chromel–alumel thermocouple. The Knudsen cell used was made of 15 mol% calcia stabilized zirconia (CSZ) with a thin cylindrical orifice of diameter 0.8 mm and height 0.2 mm at the centre of the lid. The detected signal (I_i^+) measured using a Faraday cup detector is related to the partial pressure of the vapor species (p_i) by:

$$
p_i = \frac{K_{inst} \cdot I_i^+ \cdot T}{\sigma_i \cdot a_i} \tag{1}
$$

where K_{inst} is the instrumental constant, I_i^+ is the measured ion current in ampere, T is the absolute temperature near the Knudsen cell, σ_i is the electron impact crosssection and a_i isotopic abundance of the specific ion. Eq. (1) can be represented as;

$$
\ln p_i = \ln K_{inst} + \ln(I_i^+ \cdot T) - \ln \sigma_i - \ln a_i \tag{2}
$$

Eq. (2) is used to calculate the instrument constant (K_{inst}) by calibrating with a standard having known partial pressures at different temperatures. Prior to calibration of the instrument, the background signals were monitored by heating the Knudsen cell chamber with empty Knudsen cell at different temperatures from ambient to 1161 K at pressure level ∼1 × 10[−]⁵ Pa. The background signals as a function of temperature are shown in Fig. 1. It is evident from the figure that the background signals corresponding to H_2^+ , N₂⁺, CO⁺ and CO₂⁺ do not change appreciably with change in temperature. During experiments, the actual signals were obtained by subtracting the ion intensities due to background.

The instrument was first calibrated using the phase mixture ${BaCO₃(s) + BaO(s)}$ at 30 eV ionization energy and keeping the other ion optic parameters constant for all sets of measurements. The experimental setup and the calibration constant thus calculated was checked by measuring the partial pressure of $CO₂(g)'$ ' ${p(CO₂)}$ ' over the phase mixture of ${SrCO_3(s) + SrO(s)}$. After validation of the method, $p(CO_2)$ were measured over the equilibrium phase mixtures of ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}$ and ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$. There are two ways to prepare $Sr₂CeO₄(s)$: (i) by mixing stoichiometric ratios of $S₂(s)$ and $C₂(s)$ and (ii) by successive addition of $SrCO₃(s)$ in $SrCeO₃(s)$. Hence, the values of $p(CO₂)$ were measured over both the equilibrium phase mixtures of ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)}.$

3. Results and discussion

3.1. Calibration of KEQMS setup

The individual ion intensities of CO $_2^{\mathrm{+}}$ peak over the equilibrium phase mixture of ${BaCO₃(s) + BaO(s)}$ were recorded at different temperatures for two successive runs and tabulated in [Table 1. T](#page-2-0)he individual ion intensities were least squares fitted as a function of temperature and is represented as:

$$
\ln(IT) = \frac{-31541 \left(\pm 414\right)}{T} + 15.94 \left(\pm 0.44\right) \quad (852 - 1029 \text{ K}) \tag{3}
$$

Values of $ln(K_{inst})$ as a function of temperature were calculated using Eqs. (2) and (3), the $CO₂(g)$ pressure for the equilibrium mixture ${BaCO₃(s) + BaO(s)}$ from literature [\[17\]](#page-6-0) and $\ln{\{\sigma(i = C_2)\}} = -45.52$ at 30 eV. The expression for $\ln(K_{inst})$ as a function of temperature is represented as:

$$
\ln(K_{inst}) = \frac{-12}{T(K)} - 42.02\tag{4}
$$

The ion intensities of CO_2^+ over {SrCO₃(s) + SrO(s)} were measured as a function of temperature and are given in [Table 1. T](#page-2-0)he individual ion intensities were least squares fitted as a function of temperature and are represented as:

$$
\ln(1) = \frac{-29426(\pm 641)}{T} + 15.50(\pm 0.71) \quad (849 - 965 \text{ K}) \tag{5}
$$

Fig. 1. Background mass spectra at different temperature using KEQMS with empty Knudsen cell.

Table 1

			Ion intensities of CO ₂ ⁺ peak over equilibrium phase mixtures as a function of temperature.
--	--	--	--------------------------------------------------------------------------------------------------------------------

The values of $ln{p(CO_2 \text{ (atm)})}$ for the phase mixture ${SrCO₃(s) + SrO(s)}$ was calculated by using Eqs. [\(2\), \(4\) and](#page-1-0) [\(5\). T](#page-1-0)he corresponding expression is given as:

$$
\ln\{p(CO_2(\text{atm}))\} = \frac{-29438\left(\pm 763\right)}{T} + 19.00(\pm 0.84) \quad (849 - 965 \text{ K})
$$
\n
$$
\tag{6}
$$

The $CO₂(g)$ pressure was generated over this phase mixture due the equilibrium reaction:

$$
SrCO3(s) = SrO(s) + CO2(g)
$$
\n(7)

The enthalpy change associated with reaction (7) at the average experimental temperature was calculated using Eq.(6) and found to be $\Delta_{\rm r}H_{\rm m}$ ° (907 K)=(245 \pm 6) kJ mol $^{-1}$, which is in good agreement with that of literature (239 kJ mol⁻¹) [\[17\].](#page-6-0)

3.2. Measurement of partial pressure of $CO₂(g)$ over equilibrium phase mixtures of strontium and barium cerates

Huang et al. [\[18\]](#page-6-0) have reported the thermodynamic data of Na₄Fe₆O₁₁(s) by measuring the partial pressure of CO₂(g) over ${2Na_2CO_3(s) + 3Fe_2O_3(s)}$ phase mixture using Knudsen effusion mass spectrometry. Similar approach was adopted in this study to determine the Gibbs energies of formation of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) by measuring the partial pressure of $CO₂(g)$ over the equilibrium phase mixtures of ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}, {SrCeO₃(s) + SrCO₃(s) + CeO₂(s)},$ ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) +}$ $SrCeO₃(s)$. After the mass spectrometric measurements, the resultant phase mixtures were analyzed by X-ray powder diffraction technique and found to contain the same phases and therefore, it was assumed that the following equilibrium reactions were established inside the Knudsen cell under experimental conditions.

$$
ACO3(s) + CeO2(s) = ACeO3(s) + CO2(g) (A = Sr, Ba)
$$
 (8)

$$
ACO3(s) + ACeO3(s) = A2CeO4(s) + CO2(g) (A = Sr)
$$
 (9)

Therefore, the measured $p(CO₂)$ corresponds to the equilibrium pressures of the above reactions.

3.2.1. $p(CO₂)$ over the phase mixtures ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}$ and ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$

The ion intensities of CO $_2^{\text{+}}$ peak due to the equilibrium reaction (8) (A = Ba, Sr) were measured as a function of temperature and are given in [Table 2. T](#page-3-0)he $p(CO_2)$ values were calculated by using the ion intensities and Eqs. [\(2\) and \(4\). T](#page-1-0)he variation of $\ln\{p(CO_2 \text{(atm)})\}$ as a function of temperature for both the ternary phase mixtures are shown in Figs. 2 and 3, respectively. The $\ln\{p(CO_2 \text{(atm)})\}$ values for

Fig. 2. Plot of $\ln\{p(CO_2)\}$ versus temperature for $\{BaCeO_3(s) + BaCO_3(s) + CeO_2(s)\}.$

both the phase mixtures for two successive runs were least squares fitted as a function of temperature and are represented below. For the phase mixture ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}$:

$$
\ln\{p(CO_2(\text{atm}))\} = \frac{-28891 \left(\pm 665\right)}{T} + 16.91 \left(\pm 0.73\right)
$$
\n
$$
(813 \le T(K) \le 1022)
$$
\n(10)

Fig. 3. Plot of $\ln\{p(CO_2)\}$ versus temperature for $\{SrCeO_3(s) + SrCO_3(s) + CeO_2(s)\}$.

For the phase mixture ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$:

$$
\ln\{p(CO_2(\text{atm}))\} = \frac{-27056 \, (\pm 390)}{T} + 17.96(\pm 0.48)
$$
\n
$$
(725 \le T(K) \le 922)
$$
\n(11)

The thermodynamic stability of $ACeO₃$ with respect to the formation of the corresponding carbonates $ACO₃$ is depicted in Fig. 4. The lines show the boundary of stable region of $ACeO₃$ (A = Ba, Sr). The thermodynamically stable region for cerates lies below the

Fig. 4. Stability region plot of $ACeO₃$ (A = Ba, Sr) with respect to $ACO₃$.

line, whereas above the line $ACeO₃$ will form $ACO₃$ and $CeO₂$ in presence of $CO₂(g)$. The figure also indicates the chemical stability order of cerates against $CO₂$ and predicts that SrCeO₃ is more stable compared to BaCe O_3 .

The enthalpy changes due to reaction (8) for $(A = Ba, Sr)$ at the average temperature of measurement were found to be $\Delta_{\rm r}H_{\rm m}$ ° (918 K) = (240 ± 6) kJ mol⁻¹ for A = Ba and $\Delta_{\rm r}H_{\rm m}$ ° $(824 K) = (225 \pm 3)$ kJ mol⁻¹ for A = Sr. The standard Gibbs energy of reaction (8) for $(A = Ba)$ is calculated as:

$$
\Delta_{\rm r} G_{\rm m}^{\circ}(T)(\text{kJ mol}^{-1})(\pm 6) = 240 - 0.1406 \cdot (T(\text{K}))
$$
\n
$$
(813 \le T(\text{K}) \le 1022)
$$
\n
$$
(12)
$$

The standard Gibbs energy of reaction (8) for $(A = Sr)$ is calculated as:

$$
\Delta_{\rm r} G_{\rm m}^{\circ}(T)(\mathrm{kJ\,mol^{-1}})(\pm 3) = 225 - 0.1493 \cdot (T(\mathrm{K}))
$$
\n
$$
(725 \le T(\mathrm{K}) \le 922)
$$
\n(13)

The standard molar Gibbs energies of formation $(\Delta_f G_m^\circ)$ of BaCeO₃(s) and SrCeO₃(s) from the elements were calculated from Eqs. (12) and (13) and the values of Δ_fG° _m(T) for CO₂(g), BaCO₃(s), $SrCO₃(s)$ and $CeO₂(s)$ given in Table 3. The corresponding expres-

Fig. 5. Comparison of $\Delta_f G_m^\circ(T)$ for BaCeO₃(s).

sions are:

$$
\Delta_f G_m^{\circ}(\text{BaCeO}_3, s, T)(kJ \, mol^{-1})(\pm 6) = -1675.3 + 0.3315 \cdot (T(K))
$$

$$
(813 \le T(K) \le 1022) \tag{14}
$$

$$
\Delta_f G_m^{\circ}(\text{SrCeO}_3, s, T)(kJ \, mol^{-1})(\pm 3) = -1690.3 + 0.3227 \cdot (T(K))
$$

$$
(725 \le T(K) \le 922) \tag{15}
$$

Scholten et al. [\[19\]](#page-6-0) have estimated the $\Delta_{\rm f} \mathsf{G}_{\rm m}{}^\circ(\mathsf{T})$ for BaCeO $_3(\mathrm{s})$ using their enthalpy increment data and other auxiliary data from the literature from 298.15 to 1500 K. The $\Delta_{\rm f}\mathrm{Gm^{\circ}(}T\mathrm{)}$ for BaCeO₃(s) from Eq. (14) are compared with that of above literature and represented in Fig. 5. The values of $\Delta_{\rm f} \mathsf{G}_{\rm m}{}^\circ (T)$ for BaCeO $_3$ (s) in this study is \sim 50 kJ mol⁻¹ more negative compared to the estimated literature values [\[19\].](#page-6-0)

Shirsat et al. [\[12\]](#page-6-0) have measured the partial pressure of $CO₂(g)$ over the phase mixture ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$ by tensimetric measurements in the temperature range 1113 K to 1184 K and calculated $\Delta_f G_m^\circ(T)$ for SrCeO₃(s). Pankajavalli et al. [\[13\]](#page-6-0) have determined the $\Delta_{\rm f}G_{\rm m}$ °(T) for SrCeO₃(s) using solid-state electrochemical cell experiments from 788 to 1142 K. The values of $\Delta_f G_m^\circ(T)$ for SrCeO₃(s) obtained in this study are compared with the values reported in literature [\[12,13\]](#page-6-0) and shown in Fig. 6. The figure shows that the $\Delta_{\rm f} \mathsf{G}_{\rm m}{}^\circ(\mathsf{T})$ for SrCeO $_3$ (s) are in good agreement with that of literature.

The Standard molar Gibbs energy of formation $(\Delta_f G_m^\circ)$ of $BaCeO₃(s)$ and $SrCeO₃(s)$ obtained in this study and the data reported in the literature are used to calculate the Gibbs energy change for reaction: $ACeO₃(s) + CO₂(g) = ACO₃(s) + CeO₂(s)$ and are compared in Table 4. It is observed that for A = Ba, the values of $\Delta_{\rm r}$ G_m $^{\circ}$ obtained in this study is ~60 kJ mol^{−1} more negative than that of Scholten et al. [\[19\], w](#page-6-0)hereas the values are in close agreement for $A = Sr$.

Table 4

Comparison of Gibbs energy change for reaction: $ACeO₃(s) + CO₂$ $(g) = ACO₃(s) + CeO₂(s).$

Reaction	$\Delta_{r}G_{m}^{\circ}(T)$ (k[mol ⁻¹)	Reference
$A = Ba$	$-240.0 + 0.1406$ (T(K)) $-210.8 + 0.1713 (T(K))$	This study Scholten et al. [19]
$A = Sr$	$-225.0 + 0.1493 (T(K))$ $-211.6 + 0.1445(T(K))$ $-235.0 + 0.1620 (T(K))$	This study Pankajavalli et al. [13] Shirsat et al. [12]

Fig. 6. Comparison of $\Delta_f G_m^\circ(T)$ for SrCeO₃(s).

3.2.2. $p(CO₂)$ over the phase mixtures ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)}$

Two different phase mixtures ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$ and ${Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)}$ were chosen for KEQMS experiments. After the KEQMS experiments, the resultant samples were characterized by X-ray diffraction technique and found to be the same mixture as taken before the experiments. Hence, the equilibrium reactions for both the phase mixture can be written as:

$$
2SrCO3(s) + CeO2(s) = Sr2CeO4(s) + 2CO2(g)
$$
 (16)

$$
SrCO3(s) + SrCeO3(s) = Sr2CeO4(s) + CO2(g)
$$
 (17)

The ion intensities of CO_2^+ peak due to the above equilibrium reactions were measured as a function of temperature and are given in [Table 5. T](#page-5-0)he $p(CO_2)$ values were calculated using the ion intensi-ties data from Table 4 and Eqs. [\(2\) and \(4\). T](#page-1-0)he variation of $\ln\{p(CO_2)\}$ (atm))} as a function of temperature for both the ternary phase mixtures are shown in Figs. 7 and 8, respectively. The $\ln\{p(CO_2)\}$ (atm))} values for both the phase mixtures for two successive runs were least squares fitted as a function of temperature and are represented as:

Fig. 7. $\ln\{p(CO_2)\}$ as a function of temperature for $\{Sr_2CeO_4(s) + 2SrCO_3(s) +$ $CeO₂(s)$.

Table 5

 $p(CO₂)$ values as a function of temperature for equilibrium phase mixtures for $Sr₂CeO₄(s)$.

${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$			${Sr2CeO4(s) + SrCO3(s) + SrCeO3(s)}$			
	T(K)	I(A)	$p(CO2)$ (atm)	T(K)	I(A)	$p(CO_2)$ (atm)
	1st run			1st run		
	746	$6.17E - 13$	$1.500E - 8$	776	$1.80E - 12$	$4.555E - 8$
	765	$1.19E - 12$	$2.968E - 8$	795	$2.87E - 12$	$7.443E - 8$
	782	$3.08E - 12$	$7.855E - 8$	813	5.59E-12	$1.483E - 7$
	796	$6.02E - 12$	$1.563E - 7$	833	$1.19E - 11$	$3.236E - 7$
	811	$1.12E - 11$	$2.964E - 7$	853	$2.63E - 11$	$7.325E - 7$
	825	$2.01E - 11$	$5.412E - 7$	873	5.79E-11	$1.651E - 6$
	840	$3.55E - 11$	$9.735E - 7$	891	$1.17E - 10$	$3.406E - 6$
	855	$6.59E - 11$	$1.840E - 6$	910	$2.41E - 10$	$7.167E - 6$
	868	$1.18E - 10$	$3.345E - 6$	931	$4.35E - 10$	$1.324E - 5$
	882	$1.93E - 10$	$5.561E - 6$	943	$7.30E - 10$	$2.251E - 5$
	897	$2.79E - 10$	$8.177E - 6$	2nd run		
	912	$4.93E - 10$	$1.469E - 5$	781	$1.26E - 12$	$3.209E - 8$
	2nd run			793	1.86E-12	$4.811E - 8$
	740	$4.61E - 13$	$1.112E - 8$	809	$3.59E - 12$	$9.476E - 8$
	756	7.80E-13	$1.922E - 8$	822	$6.59E - 12$	1.768E-7
	770	$1.55E - 12$	$3.891E - 8$	838	$1.25E - 11$	$3.420E - 7$
	770	$1.66E - 12$	$4.167E - 8$	852	$2.17E - 11$	6.037E-7
	784	$3.23E - 12$	8.259E-8	865	$3.54E - 11$	$1.000E - 6$
	799	$6.57E - 12$	$1.712E - 7$	880	$6.64E - 11$	$1.909E - 6$
	813	$1.13E - 11$	2.998E-7	895	$1.16E - 10$	$3.392E - 6$
	827	$1.99E - 11$	$5.371E - 7$	910	$1.96E - 10$	$5.829E - 6$
	838	$3.02E - 11$	$8.262E - 7$	925	$2.80E - 10$	8.466E-6
	851	$5.24E - 11$	$1.456E - 6$	938	$4.13E - 10$	$1.267E - 5$
	864	$9.27E - 11$	$2.616E - 6$	952	$7.67E - 10$	2.388E-5
	879	$1.66E - 10$	$4.766E - 6$			
	895	$2.46E - 10$	$7.194E - 6$			
	909	$3.80E - 10$	$1.129E - 5$			
	924	$7.82E - 10$	$2.362E - 5$			

For the phase mixture ${Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)}$:

$$
\ln\{p(CO_2(\text{atm}))\} = \frac{-28746(\pm 211)}{T} + 20.38(\pm 0.26)
$$

(740 \le T(K) \le 924) \t(18)

and for the phase mixture ${Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)}$:

$$
\ln\{p(CO_2(\text{atm}))\} = \frac{-28405(\pm 512)}{T} + 19.17(\pm 0.6)
$$
\n
$$
(776 \le T(K) \le 952)
$$
\n(19)

The enthalpy changes due to reactions [\(16\) and \(17\)](#page-4-0) at the average temperature of measurement were determined and found to be $\Delta_{r(16)}H_m^\circ$ (832 K)=(478 ± 4) kJ mol⁻¹ and $\Delta_{r(17)}H_m^\circ$

Fig. 8. $\ln\{p(CO_2)\}$ as a function of temperature for $\{Sr_2CeO_4(s) + SrCO_3(s) +$ $SrCeO₃(s)$.

Fig. 9. Comparison of $\Delta_f G_m^\circ(T)$ for Sr₂CeO₄(s).

 $(864 K) = (236 \pm 4) k$ mol⁻¹. The standard Gibbs energies of reactions [\(16\) and \(17\)](#page-4-0) are calculated and represented as:

$$
\Delta_{r(16)}G_{m}^{\circ}(T)(kJ \, mol^{-1})(\pm 2) = 478 - 0.3389 \cdot (T(K))
$$
\n
$$
(740 \le T(K) \le 924)
$$
\n(20)

and

$$
\Delta_{r(17)} G_m^{\circ}(T)(kJ \text{ mol}^{-1})(\pm 4) = 236 - 0.1594 \cdot (T(K))
$$
\n
$$
(776 \le T(K) \le 952)
$$
\n(21)

The Δ_f G_m \circ of Sr₂CeO₄(s) from the elements calculated using $\Delta_{r(16)}G_m$ °(T) and the values of Δ_fG_m °(T) for CO₂(g), SrCO₃(s) and $CeO₂(s)$ from [Table 3](#page-3-0) is given as:

$$
\Delta_f G_m^{\circ}(\text{Sr}_2\text{CeO}_4, \text{ s}, T)(k \text{J} \text{ mol}^{-1})(\pm 3) = -2266 + 0.3977 \cdot (T(K))
$$

$$
(740 \leq T(K) \leq 924) \tag{22}
$$

Similarly, the Δ_f G_m \circ of Sr₂CeO₄(s) from the elements calculated using $\Delta_{r(17)}G_m°(T)$ and the values of $\Delta_fG_m°(T)$ for $CO_2(g)$, SrCO₃(s) from [Table 3](#page-3-0) and for $SrCeO₃(s)$ from Eq. [\(15\)](#page-4-0) is given as:

$$
\Delta_f G_m^{\circ} (Sr_2CeO_4, s, T)(kJ mol^{-1})(\pm 4) = -2283.0 + 0.4279 (T(K))
$$

(776 $\leq T(K) \leq 952$) (23)

Pankajavalli et al. [\[13\]](#page-6-0) have determined the $\Delta_f G_m^\circ(T)$ of $Sr₂CeO₄(s)$ using solid-state galvanic cell technique from 805 to 1066 K. Shirsat et al. [\[14\]](#page-6-0) have determined the $\Delta_f G_m^\circ(T)$ of $Sr₂CeO₄(s)$ using tensimetric technique from 1035 to 1115 K. The individual values of $\Delta_{\rm f}G_{\rm m}$ °(T) for Sr₂CeO₄(s) were compared along with this study (Eqs. (22) and (23)) and shown in Fig. 9. It can be seen from Fig. 9 that values of $\Delta_f G_m^\circ(T)$ of $Sr_2CeO_4(s)$ determined from both the phase mixture using KEQMS technique are in very good agreement with that of literature [\[13,14\]. H](#page-6-0)ence, $\Delta_f G_m^\circ(T)$ of $Sr_2CeO_4(s)$ from Eqs. (22), (23) and that of literature [\[13,14\]](#page-6-0) were least squares fitted as a function of temperature and are represented as:

$$
\Delta_f G_m^{\circ}(\text{Sr}_2\text{CeO}_4, \, s, T)(kJ \, mol^{-1})(\pm 9) = -2273.0 + 0.4077 \cdot (T(K))
$$
\n
$$
(740 \le T(K) \le 1115)
$$
\n(24)

3.3. Comparison of $\Delta_f H_m^\circ$ (298.15 K) for BaCeO₃(s), SrCeO₃(s) and $Sr_2CeO_4(s)$

Scholten et al. [\[19\]](#page-6-0) have reported smoothed values of thermodynamic functions for BaCeO₃(s) based on their low temperature heat capacity data and high temperature enthalpy increment data

Fig. 10. Third law values of $\Delta_r H_m^\circ(T)$ for reactions [\(8\)](#page-2-0) (for A=Ba, Sr), [\(16\) and \(17\).](#page-4-0)

Table 6 $\Delta_f H_{\rm m}$ ° (298.15 K) of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s).

Compound	$\Delta_f H_m$ ° (298.15 K) (kJ mol ⁻¹)	Reference
BaCeO ₃ (s)	$-1644 \, (\pm 6)$ $-1686.5 \ (\pm 3.9)$ $-1690.0 (\pm 2.5)$	This study Scholten et al. [19] Cordfunke et al. [20]
SrCeO ₃ (s)	$-1685.2 \ (\pm 3)$ $-1675.3 \ (\pm 10.8)$, $-1676.3 \ (\pm 12.8)$ $-1687.1 (\pm 2.7)$ $-1685.6 \ (\pm 3.8)$	This study Pankajavalli et al. [13] Cordfunke et al. [20] Goudiakas et al. [21]
Sr ₂ CeO ₄ (s)	$-2286.1(\pm 3)$ $-2276.8(\pm 4)$ $-2293.7 (\pm 21)$ $-2272.5(\pm 7)$ $-2277.3(\pm 3)$ -2280.8 (Estimated)	This study ${Eq. (16)}$ This study ${Eq. (17)}$ Pankajvalli et al. [13] Shirsat et al. [14] Ali et al. [22] Yokokawa et al. [23]

from drop calorimetry. Pankajavalli et al. [13] have determined the $\Delta_{\rm f}H_{\rm m}$ ° (298.15 K) for SrCeO₃(s) and Sr₂CeO₄(s) based on their emf data and compared with that of literature [20,21]. Shirsat et al. [14] have determined the $\Delta_f H_{\rm m}$ ° (298.15 K) for Sr₂CeO₄(s) based on their tensimetry data and compared with that of literature [13,22,23]. In this study, $\Delta_f H_m^\circ$ (298.15 K) for BaCeO₃(s), $SrCeO₃(s)$ and $Sr₂CeO₄(s)$ were determined using 3rd law analysis by using partial pressure of $CO₂(g)$ over the equilibrium reactions (8) (for A=Ba, Sr), for reactions (16) and (17) . The auxiliary data for 3rd law calculations were taken from literature [17]. The values of $\Delta_{\rm r}H_{\rm m}$ ° (298.15 K) for the reactions [\(8\)](#page-2-0) (for A=Ba, Sr), [\(16\) and \(17\)](#page-4-0) were plotted as a function of experimental temperature and shown in Fig. 10. No systematic trend in the values of $\Delta_{\rm r}H_{\rm m}$ ° (298.15 K) was observed for all these above reactions.

Hence, the average value of $\Delta_{\rm r}H_{\rm m}$ ° (298.15 K) was used to calculate the $\Delta_{\rm f}H_{\rm m}$ ° (298.15 K) for the respective compound. The average value of $\Delta_{\rm f}H_{\rm m}$ ° (298.15 K) for all the compounds is listed in Table 6 along with that of literature. These values show that the $\Delta_f H_m$ ^o (298.15 K) for BaCeO₃(s) is more positive by 42 kJ mol⁻¹ and those for $SrCeO₃(s)$ and $Sr₂CeO₄(s)$ are in very good agreement with those reported in literature.

4. Conclusions

The partial pressures of $CO_2(g)$ over the equilibrium
phase mixtures of {BaCeO₂(s)+BaCO₂(s)+CeO₂(s)} and mixtures of ${BaCeO₃(s) + BaCO₃(s) + CeO₂(s)}$ and ${SrCeO₃(s) + SrCO₃(s) + CeO₂(s)}$ were calculated at the usual fuel cell operating temperature of 900 K and found to be 2.5×10^{-7} and 5.5×10^{-6} atm, respectively. These values suggest that BaCeO₃ is more prone to form carbonate compared to $SrceO₃$. The Gibbs free energies of formation of BaCeO₃ and SrCeO₃ from their elements also indicate that $SrCeO₃$ is more stable compared to $BaCeO₃$. Third law analysis also shows that partial pressure of $CO₂(g)$ over the different phase mixtures were reliable.

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