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Thermodynamic stabilities of strontium and barium cerates using Knudsen effusion quadrupole mass spectrometry

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ABSTRACT

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Keywords: Strontium cerate Barium cerate Proton conducting oxides Solid oxide fuel cell Knudsen effusion method Quadrupole mass spectrometry Thermodynamic properties A Knudsen effusion cell coupled to a quadrupole mass spectrometer was calibrated by measuring the ion intensities of CO_2^+ peak over the phase mixture {BaCO₃(s)+BaO(s)} at different temperatures. The instrument constant (K_{inst}) was calculated by comparing the ion intensities with the partial pressure data for this phase mixture taken from the literature. Subsequently, the ion intensities of CO_2^+ peak over the phase mixture { $SrCO_3(s) + SrO(s)$ } was measured and the partial pressure of $CO_2(g)$ over this phase mixture was calculated using this instrument constant. The enthalpy of reaction ($\Delta_r H_m^{\circ}$) was calculated and compared with the literature data which was found to be in excellent agreement. After validating this method by the above measurements, the partial pressure of $CO_2(g)$ over the equilibrium phase mixtures of {BaCeO₃(s)+BaCO₃(s)+CeO₂(s)}, {SrCeO₃(s)+SrCO₃(s)+CeO₂(s)}, {Sr₂CeO₄(s)+2SrCO₃(s)+CeO₂(s)} and $\{Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)\}$ were determined as a function of temperature. These partial pressure data were used in conjunction with auxiliary thermodynamic data from the literature to determine the standard molar Gibbs energies of formations of three ternary oxides BaCeO₃(s), SrCeO₃(s) and $Sr_2CeO_4(s)$. The thermodynamic data shows that at a particular pressure of $CO_2(g)$, $BaCeO_3(s)$ is more prone to form $BaCO_3(s)$ as compared to $SrCeO_3(s)$ to form $SrCO_3(s)$. This is an important assessment since these cerates doped with rare-earths are potential proton conducting ceramic oxides used as electrolytes in solid oxide fuel cells.

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1. Introduction

Ceria based ternary oxides of barium and strontium such as $BaCeO_3(s)$ and $SrCeO_3(s)$ have gained much importance due to their wide applications in solid oxide fuel cell (SOFC), hydrogen sensors, hydrogen extractors from gas mixtures, oxygen sensors and inorganic pigments [1-5]. A SOFC system usually utilizes a solid ceramic as the electrolyte and operates at higher temperature around 800 °C. SOFCs consist of two electrodes sandwiched around a hard ceramic electrolyte such as yttria stabilized zirconia [6–9]. In SOFC, hydrogen is fed into the anode of fuel cell and oxygen from the air enters into the cell through the cathode and the overall cell reaction leads to the formation of H₂O. Depending on the type of electrolyte, SOFC can be classified into two types: (1) oxide ion conducting SOFC; (2) proton conducting SOFC. The generation of water on fuel side dilutes the fuel in oxide ion conducting electrolyte and thus decreases the efficiency of the cell. These also require very high operating temperatures (>800 °C), consume large energy which is undesirable. To overcome these problems, the concept of proton conducting ceramic oxides has gained much importance as an electrolytic medium. Out of various options, rare-earth doped $SrCeO_3(s)$ and $BaCeO_3(s)$ are found to have high proton conductivities in moist environment. The proton conduction in these ceramic oxides arises due to defect reactions. Proton defects in the oxide are created when the oxide containing oxygen ion vacancies dissociate and absorb water from a surrounding wet atmosphere. In proton conducting SOFCs, water is formed on cathode, i.e. on air side, therefore, dilution of fuel does not occur and operating temperature of these cell is also low compared to oxide ion conducting SOFCs. These proton conducting ceramics such as BaCeO₃(s) and SrCeO₃(s) are very prone to form carbonates even with low concentration of CO₂(g) which in turn decreases their stability. Sr₂CeO₄ has luminescence properties when excited with UV light, cathode rays and X-rays [10]. It has also been established that un-doped and doped $Sr_2CeO_4(s)$ act as efficient blue-white and red phosphor materials [11].

A large number of literature reports are available related to the synthesis and thermodynamic stability of these cerates with respect to their constituent binary oxides [12–15]. But, the stability of these cerates has not been determined with respect to their carbonate formation. In this study, an attempt has been made to study the stability of $BaCeO_3(s)$, $SrCeO_3(s)$ and $Sr_2CeO_4(s)$ with respect

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to their carbonate formation using Knudsen Effusion Quadrupole Mass Spectrometry (KEQMS).

2. Experimental

2.1. Materials preparation

BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) were prepared using conventional solid state reaction method. Stoichiometric proportions of BaCO₃(s), SrCO₃(s) (LEICO Industries Inc., USA, mass fraction 0.9999) and CeO₂(s) (Indian Rare Earths Ltd., India, mass fraction 0.999) were homogenously mixed using an agate mortar and pestle. The mixtures were pelletized using a tungsten carbide lined steel die at a pressure of 20MPa. The pellets were first heated at 1100 K for 24 h. Then, the resultant products were ground, again pelletized and further heated at 1200 K for 48 h. The individual compounds were characterized by X-ray powder diffraction technique using STOE powder diffractometer with Cu K α radiation and graphite monochromator and found to be pure crystalline phases of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s).

Chemical analysis of all the synthesized samples was carried out using EDXRF method. The alkaline earth to cerium metal ratio obtained from EDXRF analysis was found to be the same as the formula ratio indicating that the compounds are stoichiometric with respect to metals.

2.2. Knudsen effusion quadrupole mass spectrometry (KEQMS)

In this study, a Residual Gas Analyzer (RGA) based on quadrupole mass spectrometer coupled to a Knudsen effusion system was used for equilibrium partial pressure measurements. The details of the experimental setup and the calibration procedure of the experimental setup have been described by Rakshit et al. [16]. The temperature near the Knudsen cell was measured using a pre-calibrated (ITS-90) chromel–alumel thermocouple. The Knudsen cell used was made of 15 mol% calcia stabilized zirconia (CSZ) with a thin cylindrical orifice of diameter 0.8 mm and height 0.2 mm at the centre of the lid. The detected signal (I_i^+) measured using a Faraday cup detector is related to the partial pressure of the vapor species (p_i) by:

$$p_i = \frac{K_{inst} \cdot I_i^+ \cdot T}{\sigma_i \cdot a_i} \tag{1}$$

where K_{inst} is the instrumental constant, I_i^+ is the measured ion current in ampere, T is the absolute temperature near the Knudsen cell, σ_i is the electron impact crosssection and a_i isotopic abundance of the specific ion. Eq. (1) can be represented as;

$$\ln p_i = \ln K_{inst} + \ln(I_i^+ \cdot T) - \ln \sigma_i - \ln a_i$$
⁽²⁾

Eq. (2) is used to calculate the instrument constant (K_{inst}) by calibrating with a standard having known partial pressures at different temperatures. Prior to calibration of the instrument, the background signals were monitored by heating the Knudsen cell chamber with empty Knudsen cell at different temperatures from ambient to 1161 K at pressure level ~1 × 10⁻⁵ Pa. The background signals as a function of temperature are shown in Fig. 1. It is evident from the figure that the background signals corresponding to H₂⁺, N₂⁺, CO⁺ and CO₂⁺ do not change appreciably with change in temperature. During experiments, the actual signals were obtained by subtracting the ion intensities due to background.

The instrument was first calibrated using the phase mixture $\{BaCO_3(s) + BaO(s)\}$ at 30 eV ionization energy and keeping the other ion optic parameters constant for all sets of measurements. The experimental setup and the calibration constant thus calculated was checked by measuring the partial pressure of $CO_2(g)$ ' $\{p(CO_2)\}$ ' over the phase mixture of $\{SrCO_3(s) + SrO(s)\}$. After validation of the method, $p(CO_2)$ were measured over the equilibrium phase mixtures of $\{BaCeO_3(s) + BaCO_3(s) + CeO_2(s)\}\$ and $\{SrCeO_3(s) + SrCO_3(s) + CeO_2(s)\}$. There are two ways to prepare $Sr_2CeO_4(s)$: (i) by mixing stoichiometric ratios of $SrCO_3(s)$ and $CeO_2(s)$ and (ii) by successive addition of $SrCO_3(s)$ in $SrCeO_3(s)$. Hence, the values of $p(CO_2)$ were measured over both the equilibrium phase mixtures of $\{Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)\}\$ and $\{Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)\}$.

3. Results and discussion

3.1. Calibration of KEQMS setup

The individual ion intensities of CO_2^+ peak over the equilibrium phase mixture of {BaCO₃(s)+BaO(s)} were recorded at different temperatures for two successive runs and tabulated in Table 1. The individual ion intensities were least squares fitted as a function of temperature and is represented as:

$$\ln(IT) = \frac{-31541\,(\pm 414)}{T} + 15.94\,(\pm 0.44) \quad (852-1029\,\mathrm{K}) \tag{3}$$

Values of $\ln(K_{inst})$ as a function of temperature were calculated using Eqs. (2) and (3), the CO₂(g) pressure for the equilibrium mixture {BaCO₃(s)+BaO(s)} from literature [17] and $\ln\{\sigma(i=CO_2)\}=-45.52$ at 30 eV. The expression for $\ln(K_{inst})$ as a function of temperature is represented as:

$$\ln(K_{inst}) = \frac{-12}{T(K)} - 42.02 \tag{4}$$

The ion intensities of CO_2^+ over {SrCO₃(s)+SrO(s)} were measured as a function of temperature and are given in Table 1. The individual ion intensities were least squares fitted as a function of temperature and are represented as:

$$\ln(IT) = \frac{-29426(\pm 641)}{T} + 15.50(\pm 0.71) \quad (849 - 965 \,\mathrm{K}) \tag{5}$$



Fig. 1. Background mass spectra at different temperature using KEQMS with empty Knudsen cell.

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Table 1

on intensities of CO ₂	+ peak over	equilibrium	phase mixtures	as a function of	temperature.
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$\{BaCO_3(s) + BacO_3(s) + Bac$	aO(s)}			${SrCO_3(s) + Si}$	${SrCO_3(s) + SrO(s)}$		
T (K)	<i>I</i> (A)	<i>T</i> (K)	<i>I</i> (A)	<i>T</i> (K)	<i>I</i> (A)	<i>T</i> (K)	<i>I</i> (A)
1st run		2nd run		1st run		2nd run	
852	1.04E-12	864	1.59E-12	849	8.08E-12	856	7.42E-12
876	1.99E-12	891	3.93E-12	864	1.04E-11	869	1.07E-11
896	3.85E-12	905	6.78E-12	878	1.60E-11	884	1.82E-11
942	2.33E-11	949	3.41E-11	922	8.47E-11	927	8.95E-11
952	3.31E-11	963	5.86E-11	935	1.41E-10	941	1.62E-10
968	6.03E-11	975	8.76E-11	950	2.13E-10	957	2.35E-10
981	9.03E-11	990	1.52E-10	960	2.96E-10	965	3.34E-10
993	1.37E-10	1003	2.12E-10				
1000	1.70E-10	1018	2.86E-10				
1020	2.70E-10	1027	3.57E-10				
1029	4.00E-10						

The values of $ln\{p(CO_2 (atm))\}$ for the phase mixture $\{SrCO_3(s)+SrO(s)\}$ was calculated by using Eqs. (2), (4) and (5). The corresponding expression is given as:

$$\ln\{p(\text{CO}_2(\text{atm}))\} = \frac{-29438(\pm 763)}{T} + 19.00(\pm 0.84) \quad (849 - 965 \text{ K})$$
(6)

The CO₂(g) pressure was generated over this phase mixture due the equilibrium reaction:

$$SrCO_3(s) = SrO(s) + CO_2(g)$$
⁽⁷⁾

The enthalpy change associated with reaction (7) at the average experimental temperature was calculated using Eq. (6) and found to be $\Delta_r H_m^{\circ}$ (907 K)=(245 ± 6) kJ mol⁻¹, which is in good agreement with that of literature (239 kJ mol⁻¹) [17].

3.2. Measurement of partial pressure of $CO_2(g)$ over equilibrium phase mixtures of strontium and barium cerates

Huang et al. [18] have reported the thermodynamic data of Na₄Fe₆O₁₁(s) by measuring the partial pressure of CO₂(g) over $\{2Na_2CO_3(s)+3Fe_2O_3(s)\}$ phase mixture using Knudsen effusion mass spectrometry. Similar approach was adopted in this study to determine the Gibbs energies of formation of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) by measuring the partial pressure of CO₂(g) over the equilibrium phase mixtures of $\{BaCeO_3(s)+BaCO_3(s)+CeO_2(s)\}$, $\{SrCeO_3(s)+SrCO_3(s)+CeO_2(s)\}$, $\{Sr_2CeO_4(s)+2SrCO_3(s)+CeO_2(s)\}$ and $\{Sr_2CeO_4(s)+SrCO_3(s)+SrCO_3(s)+SrCO_3(s)+SrCO_3(s)\}$. After the mass spectrometric measurements, the resultant phase mixtures were analyzed by X-ray powder diffraction technique and found to contain the same phases and therefore, it was assumed that the following equilibrium reactions were established inside the Knudsen cell under experimental conditions.

$$ACO_3(s) + CeO_2(s) = ACeO_3(s) + CO_2(g)$$
 (A = Sr, Ba) (8)

$$ACO_3(s) + ACeO_3(s) = A_2CeO_4(s) + CO_2(g)$$
 (A = Sr) (9)

Therefore, the measured $p(CO_2)$ corresponds to the equilibrium pressures of the above reactions.

3.2.1. $p(CO_2)$ over the phase mixtures { $BaCeO_3(s) + BaCO_3(s) + CeO_2(s)$ } and { $SrCeO_3(s) + SrCO_3(s) + CeO_2(s)$ }

The ion intensities of CO_2^+ peak due to the equilibrium reaction (8) (A = Ba, Sr) were measured as a function of temperature and are given in Table 2. The $p(CO_2)$ values were calculated by using the ion intensities and Eqs. (2) and (4). The variation of $\ln\{p(CO_2 \text{ (atm)})\}$ as a function of temperature for both the ternary phase mixtures are shown in Figs. 2 and 3, respectively. The $\ln\{p(CO_2 \text{ (atm)})\}$ values for



Fig. 2. Plot of $ln\{p(CO_2)\}$ versus temperature for $\{BaCeO_3(s) + BaCO_3(s) + CeO_2(s)\}$.

both the phase mixtures for two successive runs were least squares fitted as a function of temperature and are represented below. For the phase mixture $\{BaCeO_3(s) + BaCO_3(s) + CeO_2(s)\}$:

$$ln\{p(CO_2(atm))\} = \frac{-28891 \, (\pm 665)}{T} + 16.91 (\pm 0.73)$$

$$(813 \le T \, (K) \le 1022)$$
(10)



Fig. 3. Plot of $ln\{p(CO_2)\}$ versus temperature for $\{SrCeO_3(s) + SrCO_3(s) + CeO_2(s)\}$.

Table 2
p(CO ₂) values as a function of temperature for equilibrium phase mixtures for barium and strontium cerate

$\{BaCeO_3(s) + BaCO_3(s) + CeO_2(s)\}$			$\{SrCeO_3(s) + SrCO_3(s) + CeO_2(s)\}$		
T(K)	<i>I</i> (A)	<i>p</i> (CO ₂)(atm)	<i>T</i> (K)	<i>I</i> (A)	<i>p</i> (CO ₂)(atm)
1st run			1st run		
831	1.22E-12	3.311E-8	738	3.26E-13	7.843E-9
842	1.53E-12	4.208E-8	751	5.52E-13	1.352E-8
856	2.01E-12	5.621E-8	766	8.94E-13	2.234E-8
869	2.89E-12	8.206E-8	781	1.75E-12	4.459E-8
883	4.83E-12	1.394E-7	795	3.47E-12	9.003E-8
897	7.22E-12	2.117E-7	802	4.85E-12	1.270E-7
912	1.15E-11	3.429E-7	810	6.83E-12	1.806E-7
926	1.92E-11	5.814E-7	823	1.14E-11	3.063E-7
940	3.08E-11	9.470E-7	837	1.93E-11	5.276E-7
955	5.33E-11	1.665E-6	850	3.25E-11	9.024E-7
969	8.69E-11	2.755E-6	865	5.97E-11	1.687E-6
983	1.43E-10	4.600E-6	878	1.03E-10	2.955E-6
991	1.84E-10	5.968E-6	898	1.93E-10	5.666E-6
998	2.24E-10	7.317E-6	906	2.36E-10	6.991E-6
1009	2.88E-10	9.513E-6	922	4.28E-10	1.290E-5
1022	4.09E-10	1.369E-5	2nd run		
2nd run			725	3.42E-13	8.081E-9
813	4.75E-13	1.261E-8	742	4.69E-13	1.135E-8
828	6.07E-13	1.641E-8	755	7.20E-13	1.773E-8
841	7.84E-13	2.154E-8	770	1.20E-12	3.014E-8
856	1.16E-12	3.244E-8	784	2.18E-12	5.577E-8
870	1.87E-12	5.316E-8	799	4.29E-12	1.119E-7
884	3.24E-12	9.361E-8	813	7.42E-12	1.969E-7
899	5.96E-12	1.752E-7	828	1.36E-11	3.677E-7
914	1.00E-11	2.989E-7	835	1.80E-11	4.909E-7
927	1.65E-11	5.002E-7	850	3.30E-11	9.163E-7
941	2.72E-11	8.372E-7	864	5.78E-11	1.632E-6
956	4.69E-11	1.467E-6	878	1.04E-10	2.984E-6
971	7.81E-11	2.481E-6	893	1.69E-10	4.933E-6
984	1.30E-10	4.186E-6	908	2.42E-10	7.184E-6
998	2.03E-10	6.631E-6	922	4.29E-10	1.293E-5

For the phase mixture $\{SrCeO_3(s) + SrCO_3(s) + CeO_2(s)\}$:

$$\ln\{p(\text{CO}_2(\text{atm}))\} = \frac{-27056(\pm 390)}{T} + 17.96(\pm 0.48)$$

(725 \le T (K) \le 922) (11)

The thermodynamic stability of ACeO₃ with respect to the formation of the corresponding carbonates ACO₃ is depicted in Fig. 4. The lines show the boundary of stable region of ACeO₃ (A = Ba, Sr). The thermodynamically stable region for cerates lies below the



Fig. 4. Stability region plot of ACeO₃ (A = Ba, Sr) with respect to ACO₃.

line, whereas above the line ACeO₃ will form ACO₃ and CeO₂ in presence of $CO_2(g)$. The figure also indicates the chemical stability order of cerates against CO_2 and predicts that SrCeO₃ is more stable compared to BaCeO₃.

The enthalpy changes due to reaction (8) for (A=Ba, Sr) at the average temperature of measurement were found to be $\Delta_r H_m^{\circ}$ (918 K)=(240 ± 6) kJ mol⁻¹ for A=Ba and $\Delta_r H_m^{\circ}$ (824 K)=(225 ± 3) kJ mol⁻¹ for A=Sr. The standard Gibbs energy of reaction (8) for (A=Ba) is calculated as:

$$\Delta_{\rm r} G_{\rm m}^{\circ}(T)(\rm kJ\,mol^{-1})(\pm 6) = 240 - 0.1406 \cdot (T(\rm K))$$

$$(813 \le T(\rm K) \le 1022)$$
(12)

The standard Gibbs energy of reaction (8) for (A = Sr) is calculated as:

$$\Delta_{\rm r} G_{\rm m}^{\circ}(T)(\rm kJ\,mol^{-1})(\pm 3) = 225 - 0.1493 \cdot (T(\rm K))$$

$$(725 < T(\rm K) < 922) \tag{13}$$

The standard molar Gibbs energies of formation ($\Delta_{\rm f}G_{\rm m}^{\circ}$) of BaCeO₃(s) and SrCeO₃(s) from the elements were calculated from Eqs. (12) and (13) and the values of $\Delta_{\rm f}G^{\rm o}_{\rm m}(T)$ for CO₂(g), BaCO₃(s), SrCO₃(s) and CeO₂(s) given in Table 3. The corresponding expres-

Table 3
Standard molar Gibbs energy of formation, $\Delta_f G_m^{\circ}(T)$, of different compounds used
for calculation in this study taken from literature [17].

Compound	$\Delta_{\rm f} G_{\rm m}^{\circ}(T) (\rm kJ mol^{-1}) (700-1000 \rm K)$
CO ₂ (g) BaCO ₃ (s) SrCO ₃ (s)	-394 - 0.0019·(T(K)) -1206 + 0.2546·(T(K)) -1223 + 0.2627·(T(K))
CeO ₂ (s)	$-1086 + 0.2074 \cdot (T(K))$



Fig. 5. Comparison of $\Delta_{f}G_{m}^{\circ}(T)$ for BaCeO₃(s).

sions are:

$$\Delta_{\rm f} G_{\rm m}^{\circ} (\text{BaCeO}_3, \, \text{s}, T) (\text{kJ} \, \text{mol}^{-1}) (\pm 6) = -1675.3 + 0.3315 \cdot (T(\text{k}))$$

$$(813 \le I(K) \le 1022)$$
 (14)

$$\Delta_{\rm f} G_{\rm m}^{\circ} ({\rm SrCeO}_3, \, {\rm s}, \, T) ({\rm kJ\,mol}^{-1}) (\pm 3) = -1690.3 + 0.3227 \cdot (T({\rm K}))$$

$$(725 \le T(K) \le 922)$$
 (15)

Scholten et al. [19] have estimated the $\Delta_f G_m^{\circ}(T)$ for BaCeO₃(s) using their enthalpy increment data and other auxiliary data from the literature from 298.15 to 1500 K. The $\Delta_f G_m^{\circ}(T)$ for BaCeO₃(s) from Eq. (14) are compared with that of above literature and represented in Fig. 5. The values of $\Delta_f G_m^{\circ}(T)$ for BaCeO₃(s) in this study is $\sim 50 \text{ kJ} \text{ mol}^{-1}$ more negative compared to the estimated literature values [19].

Shirsat et al. [12] have measured the partial pressure of CO₂(g) over the phase mixture {SrCeO₃(s)+SrCO₃(s)+CeO₂(s)} by tensimetric measurements in the temperature range 1113 K to 1184 K and calculated $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ for SrCeO₃(s). Pankajavalli et al. [13] have determined the $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ for SrCeO₃(s) using solid-state electrochemical cell experiments from 788 to 1142 K. The values of $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ for SrCeO₃(s) obtained in this study are compared with the values reported in literature [12,13] and shown in Fig. 6. The figure shows that the $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ for SrCeO₃(s) are in good agreement with that of literature.

The Standard molar Gibbs energy of formation ($\Delta_f G_m^\circ$) of BaCeO₃(s) and SrCeO₃(s) obtained in this study and the data reported in the literature are used to calculate the Gibbs energy change for reaction: ACeO₃(s)+CO₂(g)=ACO₃(s)+CeO₂(s) and are compared in Table 4. It is observed that for A=Ba, the values of $\Delta_r G_m^\circ$ obtained in this study is ~60 kJ mol⁻¹ more negative than that of Scholten et al. [19], whereas the values are in close agreement for A=Sr.

Table 4

Comparison of Gibbs energy change for reaction: $ACeO_3(s) + CO_2(g) = ACO_3(s) + CeO_2(s)$.

Reaction	$\Delta_{\rm r} G_{\rm m}^{\circ}(T)$ (kJ mol ⁻¹)	Reference
A = Ba	$-240.0 + 0.1406 \cdot (T(K))$ $-210.8 + 0.1713 \cdot (T(K))$	This study Scholten et al. [19]
A = Sr	$\begin{array}{l} -225.0 + 0.1493 \cdot (T(K)) \\ -211.6 + 0.1445 \cdot (T(K)) \\ -235.0 + 0.1620 \cdot (T(K)) \end{array}$	This study Pankajavalli et al. [13] Shirsat et al. [12]



Fig. 6. Comparison of $\Delta_f G_m^{\circ}(T)$ for SrCeO₃(s).

3.2.2. $p(CO_2)$ over the phase mixtures { $Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)$ } and { $Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)$ }

Two different phase mixtures $\{Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)\}\$ and $\{Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)\}\$ were chosen for KEQMS experiments. After the KEQMS experiments, the resultant samples were characterized by X-ray diffraction technique and found to be the same mixture as taken before the experiments. Hence, the equilibrium reactions for both the phase mixture can be written as:

$$2SrCO_{3}(s) + CeO_{2}(s) = Sr_{2}CeO_{4}(s) + 2CO_{2}(g)$$
(16)

$$SrCO_3(s) + SrCeO_3(s) = Sr_2CeO_4(s) + CO_2(g)$$
(17)

The ion intensities of CO_2^+ peak due to the above equilibrium reactions were measured as a function of temperature and are given in Table 5. The $p(CO_2)$ values were calculated using the ion intensities data from Table 4 and Eqs. (2) and (4). The variation of $\ln\{p(CO_2 (atm))\}$ as a function of temperature for both the ternary phase mixtures are shown in Figs. 7 and 8, respectively. The $\ln\{p(CO_2 (atm))\}$ values for both the phase mixtures for two successive runs were least squares fitted as a function of temperature and are represented as:



Fig. 7. $ln\{p(CO_2)\}$ as a function of temperature for $\{Sr_2CeO_4(s)+2SrCO_3(s)+CeO_2(s)\}$.

Table 5

 $p(CO_2)$ values as a function of temperature for equilibrium phase mixtures for $Sr_2CeO_4(s)$.

$\{Sr_2CeO_4(s)+2SrCO_3(s)+CeO_2(s)\}$		{Sr ₂ CeO	$D_4(s) + SrCO_3(s) + SrCeO_3(s)$			
	T(K)	<i>I</i> (A)	$p(CO_2)(atm)$	T(K)	<i>I</i> (A)	$p(CO_2)(atm)$
	1st run			1st run		
	746	6.17E-13	1.500E-8	776	1.80E-12	4.555E-8
	765	1.19E-12	2.968E-8	795	2.87E-12	7.443E-8
	782	3.08E-12	7.855E-8	813	5.59E-12	1.483E-7
	796	6.02E-12	1.563E-7	833	1.19E-11	3.236E-7
	811	1.12E-11	2.964E-7	853	2.63E-11	7.325E-7
	825	2.01E-11	5.412E-7	873	5.79E-11	1.651E-6
	840	3.55E-11	9.735E-7	891	1.17E-10	3.406E-6
	855	6.59E-11	1.840E-6	910	2.41E-10	7.167E-6
	868	1.18E-10	3.345E-6	931	4.35E-10	1.324E-5
	882	1.93E-10	5.561E-6	943	7.30E-10	2.251E-5
	897	2.79E-10	8.177E-6	2nd run		
	912	4.93E-10	1.469E-5	781	1.26E-12	3.209E-8
	2nd run			793	1.86E-12	4.811E-8
	740	4.61E-13	1.112E-8	809	3.59E-12	9.476E-8
	756	7.80E-13	1.922E-8	822	6.59E-12	1.768E-7
	770	1.55E-12	3.891E-8	838	1.25E-11	3.420E-7
	770	1.66E-12	4.167E-8	852	2.17E-11	6.037E-7
	784	3.23E-12	8.259E-8	865	3.54E-11	1.000E-6
	799	6.57E-12	1.712E-7	880	6.64E-11	1.909E-6
	813	1.13E-11	2.998E-7	895	1.16E-10	3.392E-6
	827	1.99E-11	5.371E-7	910	1.96E-10	5.829E-6
	838	3.02E-11	8.262E-7	925	2.80E-10	8.466E-6
	851	5.24E-11	1.456E-6	938	4.13E-10	1.267E-5
	864	9.27E-11	2.616E-6	952	7.67E-10	2.388E-5
	879	1.66E-10	4.766E-6			
	895	2.46E-10	7.194E-6			
	909	3.80E-10	1.129E-5			
	924	7.82E-10	2.362E-5			

For the phase mixture $\{Sr_2CeO_4(s) + 2SrCO_3(s) + CeO_2(s)\}$:

$$\ln\{p(\text{CO}_2(\text{atm}))\} = \frac{-28746(\pm 211)}{T} + 20.38(\pm 0.26)$$

$$(740 \le T(\text{K}) \le 924)$$
(18)

and for the phase mixture $\{Sr_2CeO_4(s) + SrCO_3(s) + SrCeO_3(s)\}$:

$$\ln\{p(\text{CO}_2(\text{atm}))\} = \frac{-28405(\pm 512)}{T} + 19.17(\pm 0.6)$$

(776 \le T (K) \le 952) (19)

The enthalpy changes due to reactions (16) and (17) at the average temperature of measurement were determined and found to be $\Delta_{r(16)}H_m^{\circ}$ (832 K)=(478 ± 4)kJ mol⁻¹ and $\Delta_{r(17)}H_m^{\circ}$



Fig. 8. $ln\{p(CO_2)\}$ as a function of temperature for $\{Sr_2CeO_4(s)+SrCO_3(s)+SrCeO_3(s)\}.$



Fig. 9. Comparison of $\Delta_f G_m^{\circ}(T)$ for Sr₂CeO₄(s).

 $(864 \text{ K})=(236 \pm 4) \text{ kJ mol}^{-1}$. The standard Gibbs energies of reactions (16) and (17) are calculated and represented as:

1

$$\Delta_{r(16)}G_{m}^{\circ}(T)(kJ \text{ mol}^{-1})(\pm 2) = 478 - 0.3389 \cdot (T(K))$$

(740 \le T(K) \le 924) (20)

and

$$\Delta_{r(17)}G_{m}^{\circ}(T)(kJ mol^{-1})(\pm 4) = 236 - 0.1594(T(K))$$

$$(776 \le T(K) \le 952)$$
(21)

The $\Delta_{f}G_{m}^{\circ}$ of Sr₂CeO₄(s) from the elements calculated using $\Delta_{r(16)}G_{m}^{\circ}(T)$ and the values of $\Delta_{f}G_{m}^{\circ}(T)$ for CO₂(g), SrCO₃(s) and CeO₂(s) from Table 3 is given as:

$$\Delta_{\rm f} G_{\rm m}^{\circ}({\rm Sr_2 CeO_4}, \, {\rm s}, \, T)({\rm kJ\,mol^{-1}})(\pm 3) = -2266 + 0.3977 \cdot (T({\rm K}))$$

$$(740 \le T(K) \le 924) \tag{22}$$

Similarly, the $\Delta_f G_m^\circ$ of Sr₂CeO₄(s) from the elements calculated using $\Delta_{r(17)}G_m^\circ(T)$ and the values of $\Delta_f G_m^\circ(T)$ for CO₂(g), SrCO₃(s) from Table 3 and for SrCeO₃(s) from Eq. (15) is given as:

$$\Delta_{\rm f} G_{\rm m}^{\circ}({\rm Sr_2CeO_4, \, s, } T)(\rm kJ\,mol^{-1})(\pm 4) = -2283.0 + 0.4279 \cdot (T(\rm K))$$

$$(776 \le T(\rm K) \le 952) \tag{23}$$

Pankajavalli et al. [13] have determined the $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ of Sr₂CeO₄(s) using solid-state galvanic cell technique from 805 to 1066 K. Shirsat et al. [14] have determined the $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ of Sr₂CeO₄(s) using tensimetric technique from 1035 to 1115 K. The individual values of $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ for Sr₂CeO₄(s) were compared along with this study (Eqs. (22) and (23)) and shown in Fig. 9. It can be seen from Fig. 9 that values of $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ of Sr₂CeO₄(s) determined from both the phase mixture using KEQMS technique are in very good agreement with that of literature [13,14]. Hence, $\Delta_{\rm f}G_{\rm m}^{\circ}(T)$ of Sr₂CeO₄(s) from Eqs. (22), (23) and that of literature [13,14] were least squares fitted as a function of temperature and are represented as:

$$\Delta_{f}G_{m}^{\circ}(Sr_{2}CeO_{4}, s, T)(kJmol^{-1})(\pm 9) = -2273.0 + 0.4077 \cdot (T(K))$$

$$(740 \le T(K) \le 1115)$$
(24)

3.3. Comparison of $\Delta_f H_m^{\circ}$ (298.15 K) for BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s)

Scholten et al. [19] have reported smoothed values of thermodynamic functions for $BaCeO_3(s)$ based on their low temperature heat capacity data and high temperature enthalpy increment data



Fig. 10. Third law values of $\Delta_r H_m^{\circ}(T)$ for reactions (8) (for A = Ba, Sr), (16) and (17).

Table 6 $\Delta_{\rm f} H_{\rm m}^{\circ}$ (298.15 K) of BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s).

Compound	$\Delta_{\rm f} H_{\rm m}{}^{\circ}$ (298.15 K) (kJ mol ⁻¹)	Reference
BaCeO ₃ (s)	$-1644 (\pm 6)$ $-1686.5 (\pm 3.9)$ $-1690.0 (\pm 2.5)$	This study Scholten et al. [19] Cordfunke et al. [20]
SrCeO ₃ (s)	$\begin{array}{l} -1685.2(\pm 3)\\ -1675.3(\pm 10.8),-1676.3(\pm 12.8)\\ -1687.1(\pm 2.7)\\ -1685.6(\pm 3.8)\end{array}$	This study Pankajavalli et al. [13] Cordfunke et al. [20] Goudiakas et al. [21]
Sr ₂ CeO ₄ (s)	-2286.1 (±3) -2276.8 (±4) -2293.7 (±21) -2272.5 (±7) -2277.3 (±3) -2280.8 (Estimated)	This study {Eq. (16)} This study {Eq. (17)} Pankajvalli et al. [13] Shirsat et al. [14] Ali et al. [22] Yokokawa et al. [23]

from drop calorimetry. Pankajavalli et al. [13] have determined the $\Delta_f H_m^{\circ}$ (298.15 K) for SrCeO₃(s) and Sr₂CeO₄(s) based on their emf data and compared with that of literature [20,21]. Shirsat et al. [14] have determined the $\Delta_f H_m^{\circ}$ (298.15 K) for Sr₂CeO₄(s) based on their tensimetry data and compared with that of literature [13,22,23]. In this study, $\Delta_f H_m^{\circ}$ (298.15 K) for BaCeO₃(s), SrCeO₃(s) and Sr₂CeO₄(s) were determined using 3rd law analysis by using partial pressure of CO₂(g) over the equilibrium reactions (8) (for A=Ba, Sr), for reactions (16) and (17). The auxiliary data for 3rd law calculations were taken from literature [17]. The values of $\Delta_r H_m^{\circ}$ (298.15 K) for the reactions (8) (for A=Ba, Sr), (16) and (17) were plotted as a function of experimental temperature and shown in Fig. 10. No systematic trend in the values of $\Delta_r H_m^{\circ}$ (298.15 K) was observed for all these above reactions. Hence, the average value of $\Delta_r H_m^\circ$ (298.15 K) was used to calculate the $\Delta_f H_m^\circ$ (298.15 K) for the respective compound. The average value of $\Delta_f H_m^\circ$ (298.15 K) for all the compounds is listed in Table 6 along with that of literature. These values show that the $\Delta_f H_m^\circ$ (298.15 K) for BaCeO₃(s) is more positive by 42 kJ mol⁻¹ and those for SrCeO₃(s) and Sr₂CeO₄(s) are in very good agreement with those reported in literature.

4. Conclusions

The partial pressures of CO₂(g) over the equilibrium phase mixtures of {BaCeO₃(s)+BaCO₃(s)+CeO₂(s)} and {SrCeO₃(s)+SrCO₃(s)+CeO₂(s)} were calculated at the usual fuel cell operating temperature of 900 K and found to be 2.5×10^{-7} and 5.5×10^{-6} atm, respectively. These values suggest that BaCeO₃ is more prone to form carbonate compared to SrCeO₃. The Gibbs free energies of formation of BaCeO₃ and SrCeO₃ from their elements also indicate that SrCeO₃ is more stable compared to BaCeO₃. Third law analysis also shows that partial pressure of CO₂(g) over the different phase mixtures were reliable.

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